

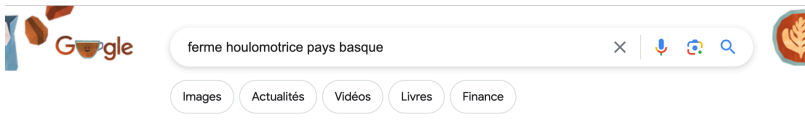
# Wave-structure interactions and wave energy

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GDR Climat

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# Don't worry...



Environ 1740 résultats (0,24 secondes)

Ce serait le projet le plus avancé en France. Une ferme houlomotrice, capable de produire a minima 30 % de l'énergie des plus de 300.000 habitants du Pays basque en 2030 : c'est l'ambition affichée mercredi à Bayonne par la région Nouvelle-Aquitaine et la Communauté d'agglomération Pays basque.




13 juil. 2023

 20 Minutes  
<https://www.20minutes.fr/planete/4045468-202307...>

[Une ferme houlomotrice en projet au large de la ... - 20 Minutes](#)

À propos des extraits optimisés • Commentaires

 Communauté Pays Basque  
<https://www.communaute-paysbasque.fr/actualite/pro...>

[Projet de ferme houlomotrice au Pays Basque](#)

13 juil. 2023 — Le site retenu pour accueillir la ferme houlomotrice est situé au large du phare de Biarritz, à une distance de 7,5 km de la côte et à une

# Wave-Energy Convertors



Diagram by Claus Lunau

# Which energy ?

## Free surface Euler equation

$$\text{(fluid domain)} \quad \begin{cases} \partial_t U + (U \cdot \nabla_{X,z})U = -\frac{1}{\rho} \nabla_{X,z} P + \mathbf{g}, \\ \operatorname{div} U = 0, \end{cases}$$

$$\text{(surface)} \quad \begin{cases} \partial_t \zeta - U \cdot N = 0, \\ P = P_{\text{atm}} \end{cases}$$

$$\text{(bottom)} \quad U \cdot N = 0$$

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$$e = \frac{1}{2} \rho g \zeta^2 + \rho \int_{b(X)}^{\zeta(t,X)} \frac{1}{2} (|V|^2 + w^2),$$

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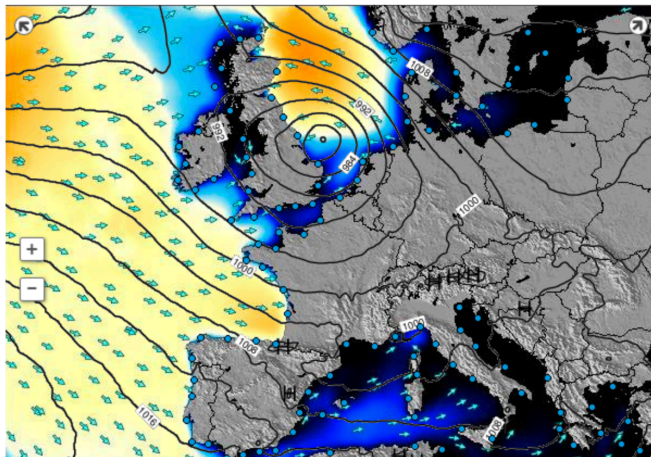
with

$$\mathcal{F} = \rho \int_{b(X)}^{\zeta(t,X)} V \left( g \zeta + \frac{1}{\rho} (P - P_{\text{atm}}) + \frac{1}{2} |U|^2 \right) \quad (\text{kW} \cdot \text{m}^{-1})$$

# Wave energy : how much ?

The annual average of wave energy in France, kilowatt/meter.


12.5 KW/m



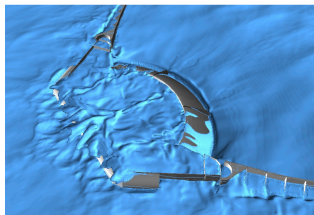


# The situation today

## Wave farms [\[ edit \]](#)

Station	Country	Location	Capacity (MW)	Type	Operation	Notes
<a href="#">Ada Foah Wave Farm</a> <sup>[1]</sup>	 Ghana		0.4	Point absorber	2016	
<a href="#">Agucadoura Wave Farm (Pelamis)</a> . <sup>[2][3]</sup> <sup>[4][5]</sup>	 Portugal	 <a href="#">41°25′57″N 08°50′33″W</a>	2.25	Surface-following attenuator	July 2008–November 2008	
<a href="#">Azura</a> <sup>[6]</sup>	 United States		0.02	Point absorber	2015	
<a href="#">BOLT Lifesaver</a> <sup>[7]</sup>	 United States		0.03	Point absorber	2016	
<a href="#">CETO</a> <sup>[8][9][10][11]</sup>	 Australia	Western Australia			2015	Two submerged buoys anchored to the seabed generate energy through hydraulic pressure.
<a href="#">Gibraltar Wave Farm</a>	 Gibraltar	Gibraltar	.1	Surface attenuator	2016	
<a href="#">Islay Limpet</a> <sup>[12][13]</sup>	 United Kingdom	 <a href="#">55°41′24″N 06°31′15″W</a>	0.5	Oscillating water column	2000–2012	
<a href="#">Mutriku Breakwater Wave Plant</a> <sup>[14][15][16]</sup>	 Spain	 <a href="#">43°18′26″N 2°23′6″W</a>	0.3 (296 kW from 16 turbines and 16 OWCs. <sup>[17]</sup> )	Oscillating water column	2011–date	Lifetime generation of over 3 GWh by the end of 2023. <sup>[18]</sup>
<a href="#">Ocean RusEnergy</a> <sup>[19]</sup>	 Russia	Yekaterinburg	N	Small-scale	2013	
<a href="#">Pico Wave Power Plant</a> <sup>[20]</sup>	 Portugal		0.4	Oscillating water column	2010	
				Oscillating		

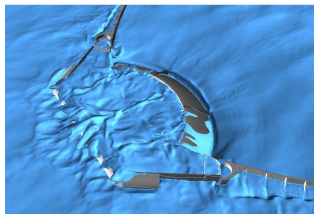
# The CFD approach



[C. Eskilsson et al. 2015]

Specific difficulties ([Kim et al 2016])

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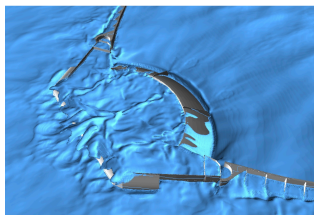


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Specific difficulties ([Kim et al 2016])

- Highly separated flow with Reynolds number  $\sim 10^7$  around hull

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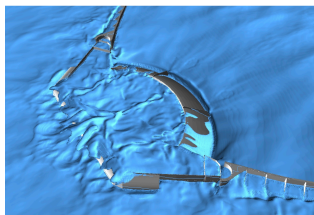


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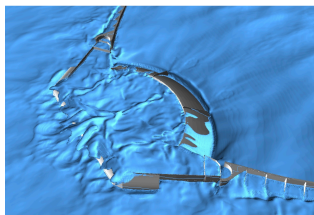


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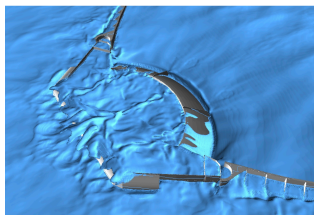


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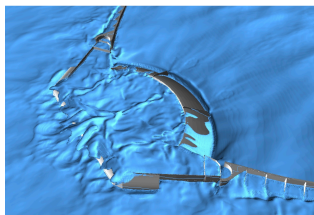


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- ↪ Cost of a CFD project for a numerical basin  $\sim$  physical model tests.

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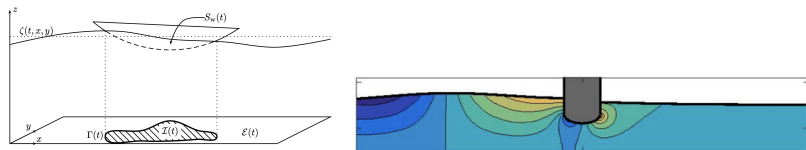
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  - Non-Gaussian stochastic environment
- ↪ Cost of a CFD project for a numerical basin  $\sim$  physical model tests.
- ↪ Relevant for
- 1 Vortex-induced motion of a multi-column floater
  - 2 Global performance of a multi-column floater in extreme wave



# Fully nonlinear potential methods



[Engsig-Karup] [Dombre et al]

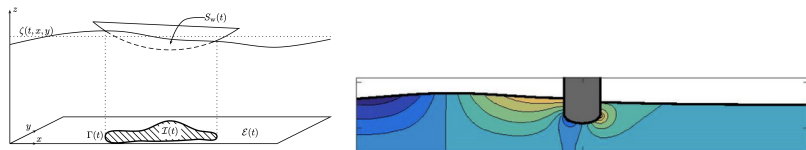
## Free surface Bernoulli equation

$$\text{(fluid domain)} \quad \begin{cases} \partial_t \Phi + gz + \frac{1}{2} |\nabla_{X,z} \Phi|^2 = -\frac{1}{\rho} (P - P_{\text{atm}}) \\ \Delta_{X,z} \Phi = 0, \end{cases}$$

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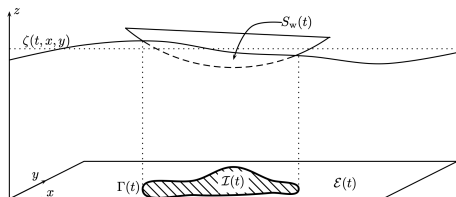
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↪ Faster than CFD but still very complicated

# Linear potential methods

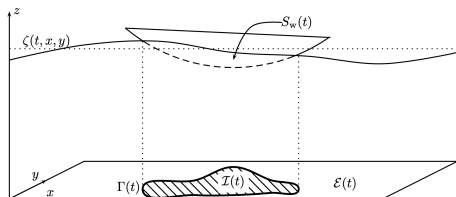


↪ The variations of the fluid domain domain are neglected

$$\Phi = \dot{x}_j \psi_j + \int_{-\infty}^t \varphi_j(t - \tau) \dot{x}_j d\tau$$

- $\psi_j$  = potential for instantaneous impulsive velocity of floating object
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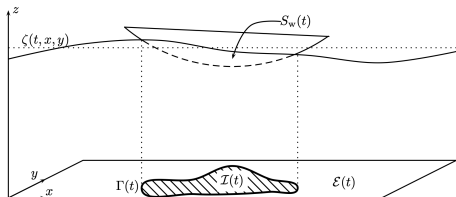
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↪ Newton:

$$m\ddot{\mathbf{x}} = m\mathbf{g} + \int_{\Gamma_w} P\mathbf{n} \sim m\mathbf{g} + \int_{\Gamma_w} (P_{\text{atm}} - \rho g z - \partial_t \Phi)\mathbf{n}$$

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↪ Cummins' equation

$$\sum_{i=1}^6 [(m_j \delta_{jk} + m_{jk}) \ddot{x}_j + c_{jk} \dot{x}_j + \int_{-\infty}^t K_{jk}(t - \tau) \dot{x}_j(\tau) d\tau] = 0 \quad (1 \leq k \leq 6)$$

# Wave-Structure interaction as partially constrained models

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(i) *Choice of the wave model.* For instance, the **NSW** equations:

$$\begin{cases} \partial_t \zeta + \nabla \cdot (h \mathbf{v}) = 0, \\ \partial_t \mathbf{v} + \mathbf{v} \cdot \nabla \mathbf{v} + g \nabla \zeta = -\frac{1}{\rho} \nabla \underline{P}, \end{cases} \quad (h = H_0 + \zeta)$$

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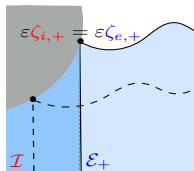
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(iii) *Matching conditions on  $\Gamma$ .* What ?

# The contacts points...

- Non-vertical walls
  - continuity of  $q$
  - continuity of  $\zeta$
  - continuity of  $\underline{P}$

↪ **free boundary problem**

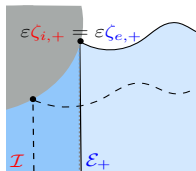


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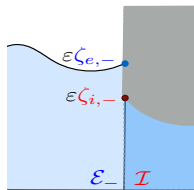
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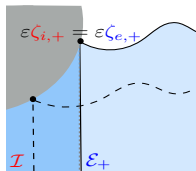


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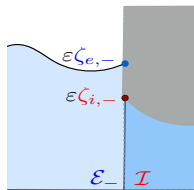
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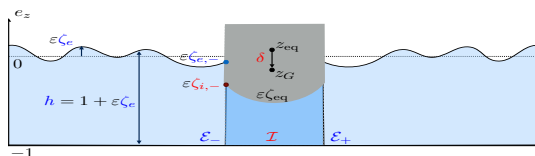
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↪ Continuity of the energy flux

# Reduction to an IBVP/ transmission problem

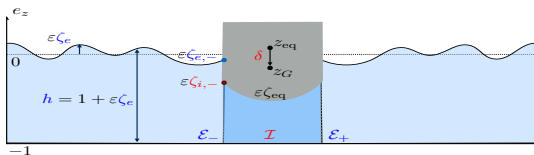


Notations:

$$[[f]] = f(\lambda) - f(-\lambda)$$

$$\langle f \rangle = \frac{1}{2}(f(\lambda) + f(-\lambda))$$

# Reduction to an IBVP/ transmission problem



- Exterior

$$\begin{cases} \partial_t \zeta_e + \partial_x q_e = 0 \\ \partial_t q_e + \partial_x \left( \frac{q_e^2}{h_e} \right) + g h_e \partial_x \zeta_e = 0 \end{cases}$$

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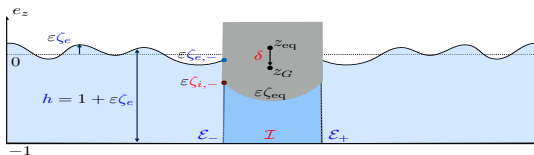
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$$\begin{cases} [[q_e]] = -2\lambda \delta, \\ \langle q_e \rangle = \langle q_i \rangle, \end{cases}$$



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where

$$\begin{cases} (m + \mathbf{m}(\delta)) \ddot{\delta} + \delta + \text{NL}(\delta, \langle q_i \rangle) = \langle \mathfrak{G}_e \rangle \\ \alpha(\varepsilon \delta) \frac{d}{dt} \langle q_i \rangle + \text{NL}(\delta, \langle q_i \rangle) = -\frac{\llbracket \mathfrak{G}_e \rrbracket}{2\lambda} \end{cases}$$

$$\mathfrak{G} := g\zeta + \frac{1}{2} \frac{q^2}{h^2}$$

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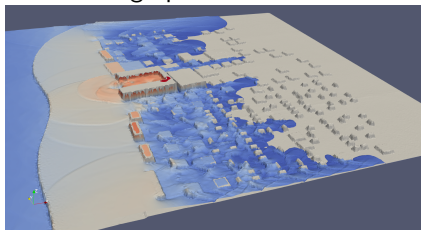
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- 3 **Constrained reduced models**
  - Limited range of validity
  - Very fast and capture nonlinear effects
  - Can be coupled to existing operational wave models



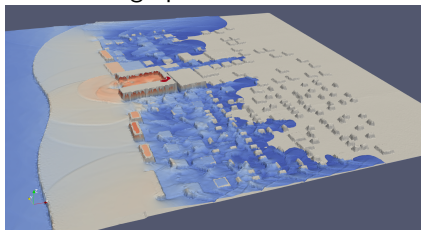
Uhaina

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# Conclusion

Various strategies:

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- 2 Fully nonlinear potential flow: precise, CPU expensive
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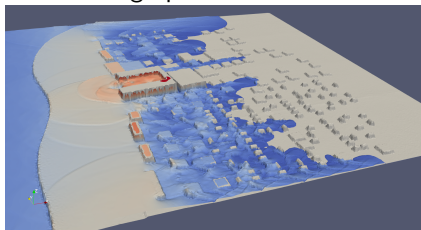
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Thank you for your attention!